The Investigation of a NZEB **Retrofit to a 1960s Head Office Building** ARCH2280 DT774b 2013-2014



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Postgraduate Diploma in **Digital Analysis and Energy Retrofit**

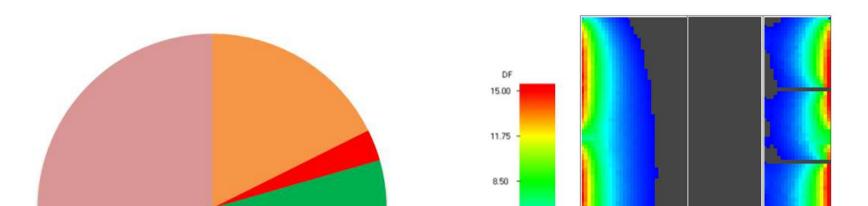
Methodology:

Annual Heating Energy Cooling Energy (Elec)

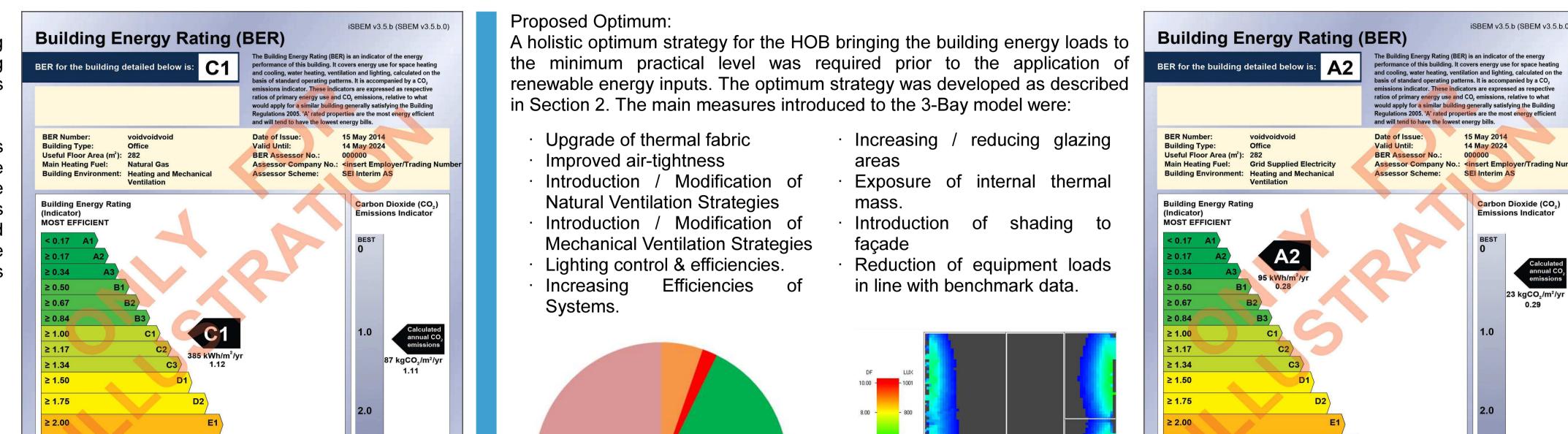
Erculation Areas existing narrow reas with storage djacent. Poor otential. Ellular Offices existing cellular

The main focus of the study was on a 3-Bay typical section of the building which represents the majority of floor space. The existing baseline building model definition is based on the geometry from the survey, building drawings provided and specifications from the investigations on site. Existing Baseline:

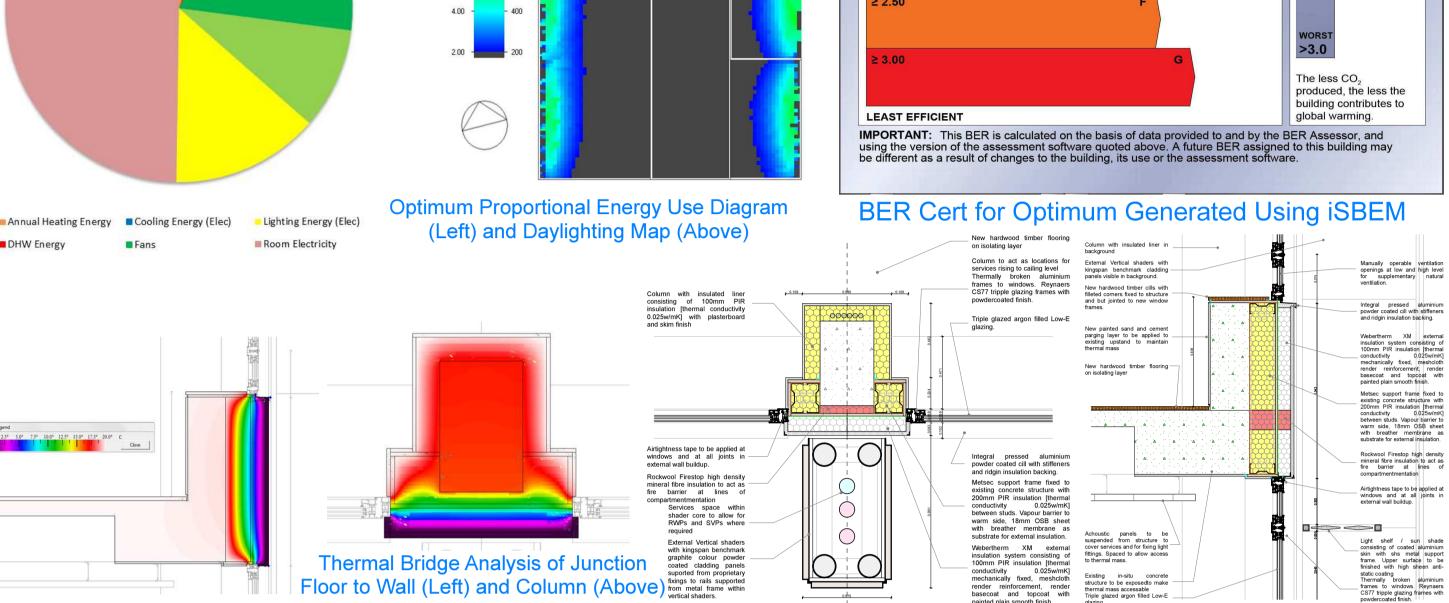
U-value and condensation risk assessments of the major envelope build-ups using the Build Desk U software and the values obtained were input into the DesignBuilder model. The software predicted that there would be some interstitial condensation and the u-values were poor. Linear thermal bridges were modelled using the Therm software and the Psi Values were calculated for the junctions. The Psi values indicate that the junctions perform quite poorly and there is likely a surface condensation risk at each of the junctions studied.



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Calculated annual CO₂ emissions



Thermal Fabric New argon filled low-E tripple glazing with thermally broken aluminium window frames. Existing plenum with 20mm

system, heating system and electrical services to be surface mounted to existing exposed in-situ concrete slabs. <u>Ceiling</u> New achoustic panels suspended from existing exposed in-situ

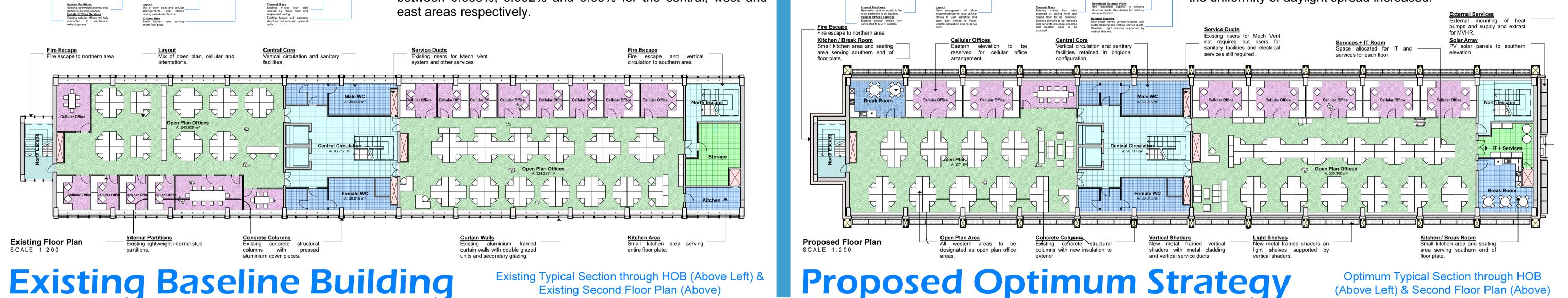
Rearranged Ancilliarry Rooms New organisation of IT + Services Rooms and Break

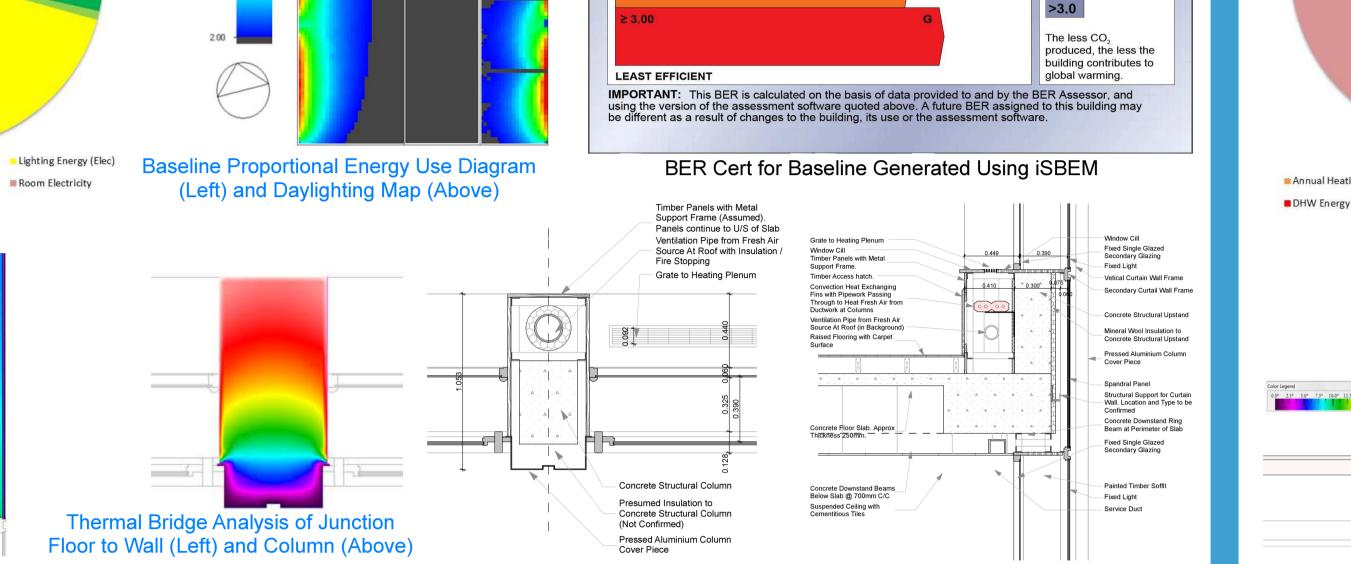
<u>Cellular Offices</u> Existing cellular offices regularised dividing walls now aligned with columns

2.25

Typical DetailsWall, Cill and Head (Above Right) & Column (Above Left)

Upon implementing these measures into the baseline energy model an optimum model was established and simulations performed. The total energy loads for this model were 14.9W/m², 14.47W/m² and 16.27W/m² for the annual, summer and winter simulations respectively. Annual Internal gains from solar $(8.83W/m^2)$, lighting $(1.94W/m^2)$ and equipment $(7.01W/m^2)$ were greatly reduced and the annual heating demand cut to 0.75W/m². The low heating The overheating and discomfort hours present in the baseline have been eliminated in the optimum simulation. Average daylighting provision generally reduced; 0.5%, 1.91% and 2.78% for the central, west and east areas respectively but the uniformity of daylight spread increased.

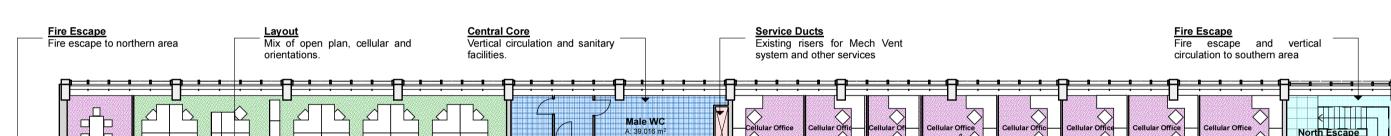




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Typical DetailsWall, Cill and Head (Above Right) & Column (Above Left)

The 3-Bay baseline model was examined using DesignBuilder for annual, summer and winter design weeks. Results were generated for energy expenditure, gains, overheating/discomfort and the daylighting provision. The total energy load was 47.57W/m² (annual), 40.33W/m² (summer) and 87.83W/m² (winter) for 3-Bay model. Internal gains from solar, lighting and equipment (13.76W/m², 20W/m² and 13.76W/m² annually) were quite high when compared to the annual heating demand (8.43W/m²). The gains contributed to the overheating which between 5.2% and 9.9% with discomfort hours between 155hours and 187hours. Average daylighting provision ranged between 0.886%, 3.952% and 5.03% for the central, west and



Comparison:

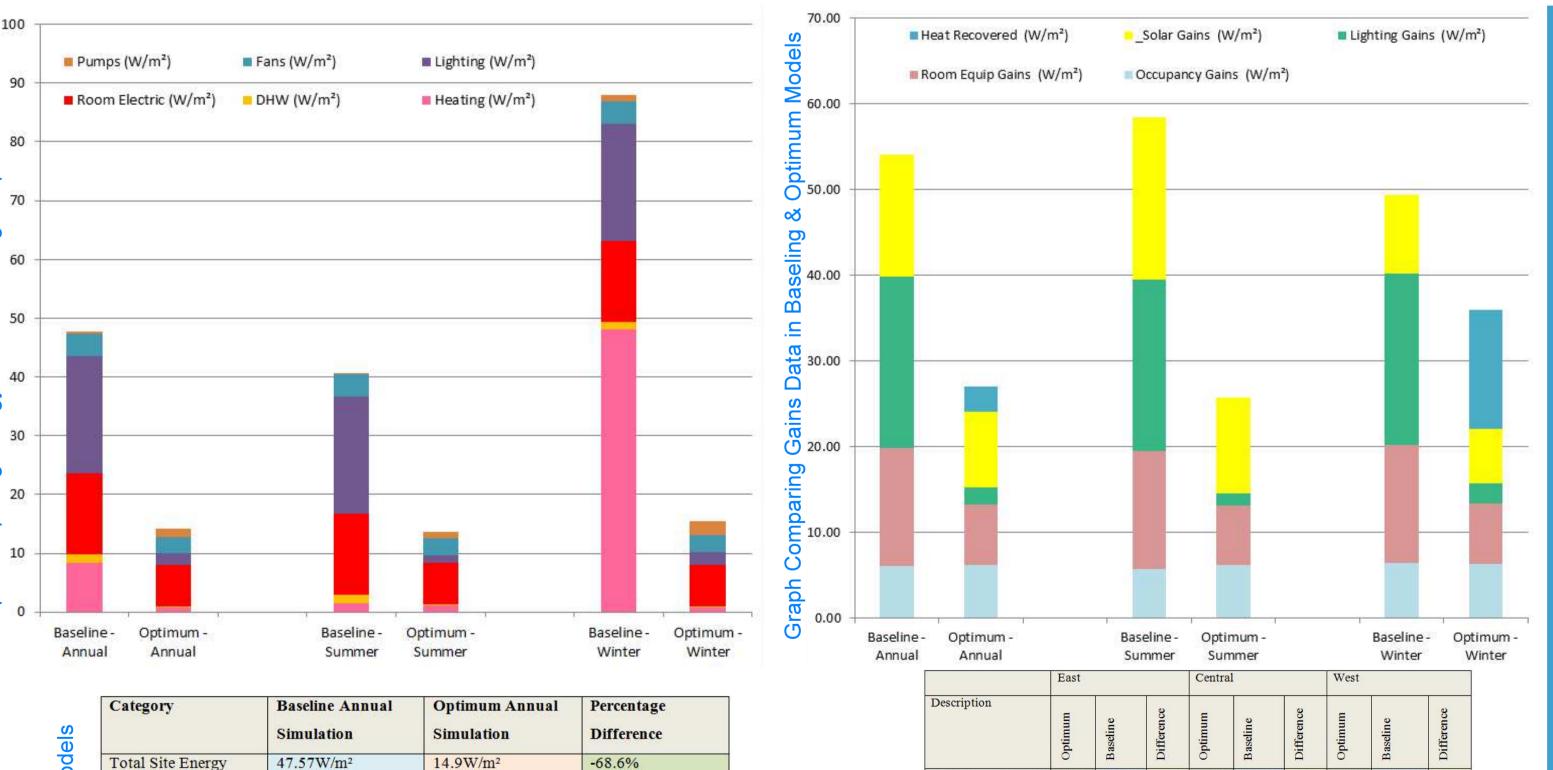
The energy balance of the simulated HOB has changed to an equipment dominant energy expenditure $\frac{3}{2}$ from the lighting dominated model that formed the baseline.

In the graph directly comparing the baseline and optimum for the different time periods examined (right), the baseline energy use is greater and in different proportions to the optimum strategy. There is also a large swing in energy use across the year on the baseline model whereas the optimum model remains 📸 quite consistent throughout.

This is also true for the graph plotting the gains data (far right). The internal gains are constantly high in the baseline results with the greatest variable being the solar gain. In the optimum model the gains are lower and at a more controlled level.

These diagrams are useful demonstrative tools and can illustrate the results in a clear and concise manner. The actual numerical savings are also vital to understanding the simulated performance of the proposed retrofit design. See table below left. As can be seen from the results in the comparison

table, the optimum retrofit strategy has reduced energy expenditure on an annual basis by 68.6%. The gains to the spaces have also been reduced by approximately 50% on an annual basis. This combined with MVHR



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NZEB:

The optimum strategy attempted to achieve the maximum practicable energy efficiency for the proposed HOB simulation. However there is still an inherent energy usage associated with the building; 14.9W/m²/annum (46kWh/m²/annum). To meet the NZEB standards renewable technologies will have to be introduced.

It is proposed to mount photovoltaic (PV) solar panels to the southern wall and roof of the retrofitted HOB with a total collector area of approximately 750m². This would provide approximately 96480 kWh /annum of electrical energy. This is approximately a quarter of the required energy demand but there is approximately 363520kWh/annum still required to achieve NZEB standards. Ideally the remainder of the renewable energy could be provided as part of a campus wide renewable energy generation strategy by, for example, a biomass CHP system. Failing the implementation of a campus wide strategy a single large wind turbine, providing approximately 0.46MWh located on the campus could fulfil the renewable energy targets for the entire HOB.

	Calculation Formula	0.80 x kWp x S x Z _{PV}
<u>a</u>		kWp = installed peak power
AL		S = annual solar radiation
From Solar Array		$Z_{PV} = overshading factor$
20	kWp/m ² of PV panel	0.15kWp/m ²
Ε	Area of Panels	750 m ²
2	Total kWp	112.5 kWp
Y	S (annual solar radiation) from	1072 kWh/m ²
	Table H2	
Energy I	ZPV (overshading factor) from	1.0
U U	Table H3	



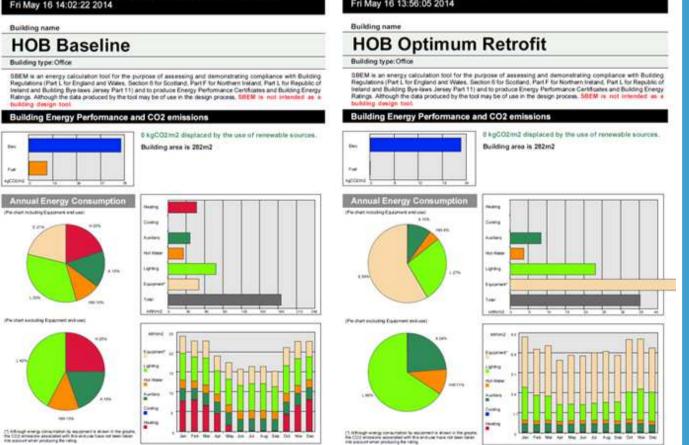
allow for a more controlled internal space removing occupant discomfort and overheating. The heating energy required for the optimum solution to be 91% lower than the baseline due to reduced demand and greater efficiency.

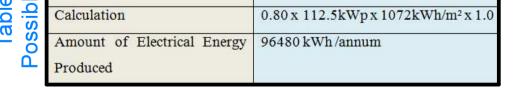
The modeled MVHR system also provided a high rate of air changes with the economiser (bypass) in operation. This in conjunction with some natural ventilation and the reduction in gains effectively eliminated overheating to the spaces. The results are compared in the table and show no hours above 28 degrees and over 90% reduction in discomfort hours. The reduction of the average daylighting provision is the only negative effect of the retrofit strategy (see graph right middle). However, the uniformity ratio of daylighting provision has increased but some supplementary artificial lighting will be required in the central area. With lighting control and efficiencies specified the predicted total lighting energy reduced by 90% in the optimum strategy.

The Building Energy Rating achieved by the baseline 3-Bay assessment of the HOB was a C1 rating and the optimum solution attained an A2 BER. iSBEM produces an illustrative BER certificate (see sections above), and advisory reports and a calculation output document, an example of which is included (far right).

Total Less Room Equipment	33.81 W/m ²	7.89W/m ²	-76.6%
Heating Energy	8.43W/m ²	0.75W/m ²	-91.1%
DHW Energy	1.39	0.27W/m ²	-80.6%
Cooling Energy	0W/m²	0W/m ²	N/A
Auxiliary Pumps	0.39W/m ²	1.33W/m ²	+243%
Auxiliary Fans	3.79W/m ²	2.79W/m ²	-26.3%
ighting Energy and Jains	20W/m ²	1.94W/m ²	-90.3%
Room Electricity and Gains	13.76W/m ²	7.01W/m ²	-49.1%
Solar Gains	14.25W/m ²	8.83W/m ²	-38%
Occupancy Gains	6.04W/m ²	6.26W/m ²	+3.6%
Heat recovered	0W/m ²	3.01W/m ²	N/A
Infiltration and Ventilation Losses	33.22W/m ²	6.72W/m ²	-79.8%
Average Fresh Air	1.90 ac/h	1.05 ac/h	-44.8%
Overheating - East	162 Hours (5.2%)	0	-100%
Discomfort - East	155 Hours	14.5 Hours	-90.7%
Overheating - Central	300 Hours (9.5%)	0	-100%
Discomfort - Central	170 Hours	13.5 Hours	-92.1%
Overheating - West	310 Hours (9.9%)	0	-100%
Discomfort - West	187.5 Hours	12 Hours	-93.6%

Average	Daylight	2.78%	5.03%	-45%	0.50%	0.886%	-44%	1.91%	3.952%	-52%
Factor				or brieffel			1017807211041			
Minimum Factor	Daylight	0.64%	1.07%	-40%	0.32%	0.454%	-29%	0.50%	0.812%	-38%
Maximum Factor	Daylight	5.93%	15.87%	-63%	0.96%	1.613%	-40%	5.44%	15.878%	-66%
Uniformity (Minimum/		0.25	0.21	+19%	0.64	0.513	+25%	0.27	0.205	+35%







Conclusions:

The learning curve in developing skills in simulation tools, specifically DesignBuilder, is quite steep and a large amount of investigation and trial and error is required. The application of single retrofit measures to the baseline model was an interesting exercise as some of the results had counterintuitive outcomes. The process was quite slow but the insight into the procedure was beneficial overall. Predictive software can be an invaluable tool in identifying possible problem areas and areas for improvement within the building design prior to construction. The investigation provided insight into passive architectural solutions, sealed mechanically ventilated systems and the holistic approach required for the optimum solution.

The single measure that had the largest impact was the lighting control, which is incidentally is the measure that could most easily be introduced in isolation and that does not have a negative impact (e.g. on overheating). Lighting control and greater efficiencies, as such, should be the first item considered for all office buildings as a priority. The internal gains present in an office building provide the greatest challenge when strategizing a retrofit solution. The levels of equipment use and occupancy gains mean that the application of a strategy that has not been considered holistically could have large negative impacts on the occupants.

NZEB & Conclusion

Comparison of Results: Baseline & Optimum